CBT-C, CB3T, and CB3Q Signal-Switch Families

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ABSTRACT

Signal-switch devices are used widely in applications requiring bus isolation, multiplexing, demultiplexing, and voltage translation. Compared to other logic and linear product alternatives, signal switches are the fastest and least power consuming. Texas Instruments (TI) CBT-C, CB3Q, and CB3T signal-switch families have low on-state resistance, negligible power consumption, and better undershoot protection, compared to the older switch families. These qualities make CBT-C, CB3Q, and CB3T devices very good candidates for today’s high-speed applications that require switches. This application report discusses some of the critical characteristics, features, and applications of TI’s newest switches.

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1 Introduction

On-off switches are one of the most common control elements in electrical circuitry. This has evolved over the years, from the manually operated circuit breaker of the early experiments to the multiscit integrated circuit of today. In every application, the function of the switch remains the same: to isolate or connect two sections of an electrical circuit. Therefore, an ideal switch should have zero resistance (short circuit) when on and infinite resistance (open circuit) when off. However, in practical applications, a bus switch should have as low resistance as possible when on, for bus connection, and as high resistance as possible when off, for bus isolation.

2 Semiconductor Switches

An insulated-gate field-effect transistor (IGFET) switch is a widely used electronic switch. A metal-oxide semiconductor field-effect transistor (MOSFET) is one type of IGFET. Although the term MOSFET is more commonly used, now most of the electronic switches do not use the metal oxide as the gate. Instead, a more advanced process is being used to form the gate. TI uses advanced poly-silicon gate-enhancement-mode transistor technology to fabricate semiconductor switches, which gives more control of performance characteristics. Throughout this application report the term MOSFET and the associated terms related to MOSFET are used because they are more common in semiconductor literature. When sufficient bias voltage is applied to the gate of a MOSFET, it creates a low-resistance path between its source and drain. When the bias voltage is removed, the resistance of this path becomes very large. MOSFETs can be of two types, n-channel MOSFET (NMOS) and p-channel MOSFET (PMOS).
2.1 NMOS Switch

The symbol of an NMOS is shown in Figure 1. The source and the drain of an NMOS are interchangeable. The terminal with the lowest voltage is considered to be the source. The resistance between the drain and the source depends on the voltage difference between the gate and the source ($V_{GS}$). When there is sufficient voltage applied to the gate with respect to the source, the switch becomes conductive, and a voltage signal applied to the drain passes through this switch without distortion. The gate-to-source voltage at which the NMOS begins conduction is known as the threshold voltage ($V_T$). If the gate-to-source voltage becomes significantly less than the threshold voltage of the NMOS ($V_T$), the channel resistance increases rapidly.

![Figure 1. NMOS](source)

2.2 PMOS Switch

A PMOS is similar to an NMOS (see Figure 2). However, to keep the source-to-drain resistance low, the difference in the source-to-gate voltage ($V_{SG}$) should be greater than the threshold voltage. In a PMOS, the terminal with the lowest voltage is considered to be the drain.

![Figure 2. PMOS](source)

3 Basic Signal-Switch Structures

Signal switches in their simplest form are MOSFET structures, with the gate driven by a CMOS inverter. Three types of structures are most common:

- NMOS series switch
- NMOS/PMOS parallel switch
- NMOS series switch, with the charge pump

3.1 NMOS Series Switch

The most basic signal-switch structure is an NMOS pass transistor, with the gate driven by a CMOS inverter. The simplified structure is shown in Figure 3.
When the output enable (ŒE) signal is low, the voltage at the gate is high, or equal to $V_{CC}$. If the voltage at the drain ($V_I$) is less than $V_{CC}$ by the threshold voltage of the n-channel transistor, the on-state resistance ($r_{on}$) is low and the voltage at the source is equal to $V_I$ ($V_O = V_I$). If $V_I$ approaches $V_{CC}$, $r_{on}$ increases rapidly, the source voltage does not increase with the drain voltage, and the output voltage remains at $V_{CC} - V_T$. A limitation of the NMOS series switch is that it can pass signals only up to a threshold voltage below $V_{CC}$. Figure 4 shows the general shape of $r_{on}$ vs $V_I$ characteristic of a typical NMOS series switch.

Figure 4. $r_{on}$ vs $V_I$ Characteristic of an NMOS Series Switch ($V_{CC} = 5$ V, $I_O = -15$ mA)

### 3.2 NMOS/PMOS Parallel Switch

An NMOS/PMOS parallel switch consists of an n-channel pass transistor in parallel with a p-channel pass transistor. Figure 5 shows the basic structure of an NMOS/PMOS parallel switch. In an n-channel MOSFET, the source-to-drain resistance is low when the drain voltage is less than $V_G - V_T$, where $V_G$ is the gate voltage. In a p-channel MOSFET, the source-to-drain resistance is low when the source voltage is greater than $V_T + V_G$. With the parallel combination of n-channel and p-channel pass transistors, the source-to-drain, or channel resistance, can be lowered for the entire input voltage range from 0 V to $V_G$. When ŒE is low, $V_G$ in NMOS/PMOS parallel switch is $V_{CC}$, and signals ranging from 0 V to $V_{CC}$ can be passed through this switch. Figure 6 shows the general shape of the $r_{on}$ vs $V_I$ characteristics of a typical NMOS/PMOS parallel switch, as well as the NMOS and PMOS characteristics. The shape of $r_{on}$ vs $V_I$ curve may be different, depending on the structures of NMOS and PMOS. The disadvantage of the NMOS/PMOS parallel switch is that the input and output capacitances increase due to the additional source and drain area of the combined transistors.
3.3 NMOS Series Switch With the Charge Pump

Although, in an NMOS/PMOS parallel switch, source-to-drain resistance is lower than in an NMOS series switch, the PMOS adds capacitance, which is undesirable for some applications. To solve this problem, another type of switch structure is used that involves a charge-pump circuit in the NMOS series switch. The charge-pump circuit generates a voltage at the gate of the NMOS that is 2 V to 3 V higher than $V_{CC}$. As a result, when the input reaches the $V_{CC}$ level, the switch still is on and the output voltage is equal to the input voltage over the 0 V to $V_{CC}$ input voltage range. The disadvantage of implementing a charge-pump circuit in the NMOS series switch is the additional power consumption because of the charge-pump circuit. Figure 7 shows a simple schematic of an NMOS series switch with the charge pump, and Figure 8 shows the $r_{on}$ vs $V_I$ characteristic.
4 Key Concerns in Digital-Switch Applications

4.1 Undershoot

Undershoot is a typical phenomenon in high-speed applications where impedance mismatches cause excessive ringing in the system. This poses a serious problem to bus switches that are turned off and attempt to isolate different buses. In this state, the gate voltage of the n-channel pass transistors are at ground potential, but a negative voltage on either I/O port with a magnitude greater than the NMOS $V_T$ will cause the switch to conduct and no longer isolate the buses. Therefore, undershoots with a large magnitude and long duration result in data corruption, if no undershoot protection circuitry is included in the signal-switch design. The schematics in Figure 9 demonstrate the phenomenon of undershoots. For normal input voltages ranging from 0 V to $V_{CC}$, the switch is in the high-impedance state and the output bus is isolated from the input bus. The undershoot produces a glitch at the isolated bus, as shown in Figure 9.
Input voltage pulse, $V_I$

Output voltage pulse, $V_O$

Output voltage stays at 3.5 V when input voltage switches from 0 to $V_{CC}$.

Gate-to-Source Voltage, $V_{GS} < 0$, switch off

Gate-to-Source Voltage, When $V_I = -2 \text{ V}$, $V_{GS} = 2 \text{ V}$, switch on

Voltage at enable input is high, i.e., $V_{CC}$

Figure 9. Undershoot in NMOS Series-Switch Devices When Disabled
There are two solutions to prevent the NMOS from turning on during the undershoot event while disabled:

- Capture or clamp the input undershoot energy. In this method, a clamp circuit is connected to ground or VCC. This clamp circuit prevents the NMOS from turning on while an undershoot event occurs.
  - Schottky Clamp. In this method, a Schottky diode is connected from the I/O port of the switch to ground. When the voltage at the I/O port goes below ground, the diode is forward biased and clamps the source or drain voltage, keeping the input and output isolated. An example of this type of device is the CBTS bus switch provided by TI.
  - Active clamp to VCC. In this method, an active clamp circuit is connected to VCC, which tries to counteract the undershoot voltage by pulling the input voltage to VCC. An example of this type of device is the CBTK bus switch provided by TI.
- Force the gate voltage of the NMOS to track the negative input voltage. TI’s new CBT-C family uses this method to prevent undershoot. This method of protection is described later in this application report.

4.2 \( r_{on} \)

\( r_{on} \) is the resistance of the switch when turned on. \( r_{on} \) should be as low as possible to reduce signal loss and to reduce propagation delay. Propagation delay of the switch depends on the RC time constant, which is made up of the switch \( r_{on} \) and the load capacitance. For applications in transmission-line environments, \( r_{on} \) should be less than, or equal to, the line impedance to minimize unwanted signal reflections. For digital applications where the switch is connected to a resistive load, the switch resistance and the load resistance form a voltage divider. Therefore, in this case, \( r_{on} \) should be as low as possible to maintain a valid input logic high (i.e., \( V_{IH} \)) of the downstream devices. \( r_{on} \) not only should be small, but also should be flat across the input voltage range to maintain a linear signal change from input to output. Signal distortion depends on the flatness of the \( r_{on} \) vs \( V_I \) curve, that is, equal to \( 20\log_{10}\Delta r_{on}/R_L \), where \( R_L \) is the load resistance. So, to keep signal distortion minimum as the signal amplitude varies, \( r_{on} \) should be kept flat over the whole input signal range. In NMOS series switches, special gate voltage-boost circuitry is needed to keep \( r_{on} \) flat over the VCC range. In NMOS/PMOS parallel switches, \( r_{on} \) is fairly constant and may have multiple peak values within 0 V to VCC input voltage range. The shape of the \( r_{on} \) vs \( V_I \) curve depends on the threshold voltages of NMOS and PMOS (see Figure 6).

4.3 \( C_{io(off)} \)

\( C_{io(off)} \) for a through switch is the off-state capacitance of one channel, measured from either the input or output of the switch. For a multiplexer or bus-exchange switch, \( C_{io(off)} \) may include off-state capacitance for multiple channels. \( C_{io(off)} \) should be as small as possible to prevent capacitive loading of the bus. Reducing \( C_{io} \) requires less drain and source area of the pass transistors that otherwise would increase on-state resistance. So, there is a trade-off between \( C_{io(off)} \) and \( r_{on} \).
4.4 $C_{\text{io(on)}}$

This is the on-state capacitance of the switch, measured from either the input or output of the switch. Usually $C_{\text{io(on)}}$ is greater than twice the $C_{\text{io(off)}}$ because it includes the capacitance on both input and output of the switch, as well as the channel capacitance. Like $C_{\text{io(off)}}$, $C_{\text{io(on)}}$ should be as small as possible to reduce capacitive loading of the bus. Reducing $C_{\text{io(on)}}$ requires less drain and source area of the pass transistors that otherwise would increase the on-state resistance. So, like the $C_{\text{io(off)}}$, there is a trade-off between $C_{\text{io(on)}}$ and $r_{\text{on}}$.

4.5 $C_{i}$ (Control Input Capacitance)

When switching control input, a large control input capacitance will inject more charge to the gate of the pass transistor. This will cause crosstalk and degrade performance of the switch.

4.6 Leakage Current

Leakage current during the high-impedance state should be very small. Leakage current, if high, may load an isolated bus and corrupt the data.

4.7 Enable and Disable Delays

Enable and disable delays are measures of how quickly the switch can be turned on and off. Not only should these delays be as small as possible for high-speed operation, but also the difference of enable and disable delays should be as small as possible to reduce the current flow between the off switch and on switch. This is significant in multiplexing and demultiplexing operations where the difference, if large, can cause bus contention. For break-before-make functions, disable time should be less than enable time and for make-before-break functions, enable time should be less than disable time.

4.8 Partial Power Down

Today’s high-speed applications require that a device can be powered-down while still connected to a live bus. This requires the switch to be in the high-impedance state while the power is down. A special $I_{\text{off}}$ circuit is incorporated to ensure that the switch is in the high-impedance state while the power is off. $I_{\text{off}}$ circuitry prevents damaging current backflow through the device when it is powered down.

4.9 Voltage Translation

One popular application of the bus switch is voltage translation in a mixed-voltage environment. A simple NMOS can pass a signal from 0 V to $V_{\text{CC}} - V_T$, where $V_T$ is the threshold voltage of the NMOS. This characteristic can be used for down translation. Figure 10 shows an example of 5-V to 3.3-V translation using an NMOS series switch, diode, and resistors.
5 Signal Switch Families from TI

TI offers a wide variety of signal switches suitable for many different types of applications. Some of the signal-switch families are discussed in the following sections:

- CBT-C: 5-V NMOS switches with \(-2\)-V undershoot protection
- CB3Q: NMOS switches with a charge-pump circuit for low and flat \(r_{on}\)
- CB3T: Level-shifting NMOS bus switch

CBT-C and CB3Q devices can pass digital and analog signals.

5.1 CBT-C Family

The switches of this family are NMOS series switches. The operating \(V_{CC}\) of this family is 5 V, and switching for various standards (i.e., LVCMOS, LVTTL etc.) can be accomplished. This family also has an undershoot protection circuit integrated in the bus switch. The undershoot protection circuit prevents the n-channel pass transistor from turning on when the switch is off. When undershoot occurs, this circuit senses the negative voltage at the input and biases the gate of the n-channel pass transistor to that negative voltage. Since the gate and source voltage are now at the same potential (<0 V), the switch remains off. Undershoot protection on one side of the off switch can prevent up to \(-2\) V undershoots on the other side of the switch. Static power consumption of this family is negligible. Dynamic power consumption depends on the frequency of the enable input of the device. Switching high and low at the enable input causes internal CMOS inverters to switch between low and high; therefore, a higher frequency of the control input signal results in higher dynamic power consumption. Undershoot protection in CBT-C is shown in Figure 11.
5.1.1 Characteristics of the CBT-C Family

The following paragraphs discuss some of the critical performance characteristics of the CBT16211C. The setup for measurements is given in Appendix A.

Figure 11. Undershoot Protection in CBT-C When Enable Input (OE) Voltage is High
5.1.1.1 \( V_O \) vs \( V_I \)

Figure 12 shows the output-voltage vs input-voltage characteristics of the CBT16211C at an output load of 3 kΩ to ground. The output follows the input approximately until 3.5 V and remains flat as the switch begins to turn off. Output voltage also depends on the output current. If output current increases, the output voltage will become flat at a lower input voltage.

![Figure 12. \( V_O \) vs \( V_I \) at \( V_{CC} = 5 \text{ V} \)](image)

5.1.1.2 \( r_{on} \) vs \( V_I \)

Figure 13 shows the switch resistance (\( r_{on} \)) when on, as a function of the input voltage. The output current is –15 mA. The on-state resistance is low when the input voltage is below 3.5 V and increases rapidly above 3.5 V. \( r_{on} \) depends on the output current and increases rapidly at a lower input voltage when the output current increases.

![Figure 13. \( r_{on} \) vs \( V_I \) at \( V_{CC} = 5 \text{ V} \) (\( I_O = -15 \text{ mA} \))](image)

5.1.1.3 Undershoot Protection

Figure 14 shows the undershoot protection performance of the CBT16211C when the switch is disabled. The output pin is connected to ground through a 100-kΩ resistor, a 10-pF capacitor, and to 10 V through a 100-kΩ pullup resistor. The test load is similar to a high-impedance application load. There is very little variation in output voltage caused by input-voltage undershoot.
5.1.2 Application of CBT-C Family

5.1.2.1 Bus Isolation

CBT-C devices can be used for 5-V PCI bus isolation for hot-plug applications (see Figure 15). PCI is an unterminated interface; therefore, undershoot may occur. CBT-C provides good isolation when an undershoot event occurs.
Figure 15. Example of Bus Isolation Using a CBT-C Device

NC – No internal connection
5.2 CB3Q Family

The switches of this family are NMOS only, with a low and flat $r_{on}$. The flat characteristics of $r_{on}$ are accomplished by a charge-pump circuit that generates a voltage of approximately 7 V at the gate of the n-channel pass transistor. As a result, 0-V to 5-V rail-to-rail switching can be accomplished because the gate-to-source voltage is well above the threshold of the n-channel transistor, and the switch is completely on over the whole 0-V to 5-V range. An internal oscillator circuit is a part of the charge-pump circuit; therefore, static power consumption of this family is higher than the CBT-C family. Dynamic power consumption depends on the frequency of the enable input. In addition to the low and flat $r_{on}$ characteristics, this family has low input and output capacitance, making them suitable for high-performance applications. The maximum switching frequency for I/O signals depends on various factors, such as type of load, input-signal magnitude, input-signal edge rates, type of package, etc. With a larger package, the inductance and capacitance can form a resonant circuit that may cause phase and magnitude distortion. With a large capacitive load, the RC time constant becomes higher and limits the frequency. Figure 16 shows a simplified schematic of a CB3Q device.

Figure 16. Simplified Schematic of a CB3Q Device

5.2.1 Characteristics of the CB3Q Family

Following sections discuss some of the critical performance characteristics of the CB3Q3306A. The measurements setup can be found in Appendix A.

5.2.1.1 $V_O$ vs $V_I$

Figures 17 and 18 show the $V_O$ vs $V_I$ characteristics of the CB3Q3306A at different values of $V_{CC}$ and at different temperatures. For $V_{CC} = 3.6$ V, the output exactly follows the input from 0 V to 5 V. Because of this characteristic, CB3Q devices can be used for switching analog and digital signals, ranging from 0 V to 5 V. For $V_{CC} = 2.3$ V, the gate voltage produced by the charge-pump circuit is reduced to about 4 V. So, the output approximately follows the input from 0 V to 3.3 V and becomes constant above 3.3 V.
5.2.1.2 \( r_{on} \) vs \( V_I \)

The CB3Q3306A has low and flat \( r_{on} \) characteristics. Figure 19 and Figure 20 show \( r_{on} \) vs input voltage characteristics at different values of \( V_{CC} \) and at different temperatures. The output current for \( r_{on} \) vs \( V_I \) characteristics is \(-15\) mA, and this characteristic is dependent on output current. For \( V_{CC} = 3.6\) V, \( r_{on} \) is fairly constant from the 0-V to 5-V input-voltage range. For \( V_{CC} = 2.3\) V, \( r_{on} \) is flat over the range of 0 V to 2.5 V and increases rapidly above 2.5 V.
5.2.1.3 Operation at High Frequency

Low input and output capacitance, low $r_{on}$, and low feed-through capacitance makes the CB3Q devices suitable for high-speed applications. Maximum frequency of operation depends on input voltage range, type of load, edge rate, type of package, off-isolation, crosstalk requirement, etc. At high frequencies, off-isolation and crosstalk also increase, which limits the maximum frequency of operation. Figure 21 shows the input and output voltage waveforms at a frequency of 420 MHz, with a 500-Ω and 3-pF load. From Figure 21, it is clear that the switch, when on, allows high-frequency signals to pass without distortion. Also, the switch provides very good isolation between the input and output when it is turned off or disabled.

![Figure 21. Input and Output Voltage Waveforms for the CB3Q3306A at 420 MHz (VCC = 3.3 V)](image-url)
5.2.1.4 Output Skew

Output skew is a measure of the variation of $r_{on}$ over the channels in a multibit switch. This is specifically significant when switching differential signals. For minimal signal distortion and noise in differential signaling, the variation of $r_{on}$ should be as small as possible. Output skew at a specific voltage can be determined by measuring the time difference of the output voltage at various channels. Figure 22 and Figure 23 show the output voltage of the CB3Q3306A at different channels. Output skew can be determined from this graph. For example, for $-40^\circ C$ at 2.5 V, the skew is approximately 30 ps, which is fairly constant from 2.2 V to 2.6 V. For 100$^\circ C$, the output skew is approximately 40 ps, which is fairly constant from 2.2 V to 2.6 V.

![Figure 22. Output Skew at $-40^\circ C$ ($V_{CC} = 3.3$ V)](image)

![Figure 23. Output Skew at 100$^\circ C$ ($V_{CC} = 3.3$ V)](image)
5.2.1.5 Frequency Response

Figure 24 and Figure 25 show the attenuation and off-isolation for the CB3Q3306A at different loads as a function of frequency. The bandwidth depends on the type of load, and bandwidth decreases as the load increases.

Figure 24. Attenuation and Off-Isolation for the CB3Q3306A at 3-pF Load (V_{CC} = 3.3 V)
Figure 25. Attenuation and Off-Isolation for the CB3Q3306A at 50-pF Load ($V_{CC} = 3.3$ V)
5.2.1.6 Adjacent Channel Crosstalk

For some applications, crosstalk is an important parameter. Figure 26 shows the crosstalk between adjacent channels in the CB3Q3306A.

Figure 26. Crosstalk of the CB3Q3306A at 3-pF Load (V_{CC} = 3.3 V)
5.2.2 Application of the CB3Q Family

5.2.2.1 Multiplexer in USB Applications

Figure 27 shows a USB 2.0 application in which a bus-switch device can be used. The first switch in a notebook PC is used to isolate between a notebook PC and the docking station. The switches on the docking station are used as a multiplexer to provide two different paths for the DATA+ and DATA− signals. If the operating system is Windows 95, the USB 2.0 hub is not supported. Switches 1 and 2 are on, and the USB line is connected directly to Port 1. Figure 28 shows the use of a CB3Q3257 in this type of application.

![Figure 27. Multiplexing in a USB Application](image-url)
Figure 28. CB3Q3257 in a USB Application

DATA+ signal path is shown as a dotted line and the DATA– signal is shown as a solid line. The DATA+ signal goes to 1A. Depending on the select signal (S) levels, the output can be 1B1 or 1B2. When S is low, DATA+ from the host controller is connected to the port through the USB 2.0 hub (1A → 1B1 → USB 2.0 Hub → 3B1 → 3A → Port 1). When S is high, the DATA+ is connected to port 1 directly (1A → 1B2 → 3B2 → 3A). Similarly, DATA– uses the 2A, 2B1, 2B2 and 4A, 4B1, 4B2 switches for connecting to port 1.

5.3 CB3T Family

CB3T is a voltage-translation bus-switch family. This family can operate with a power-supply voltage range of 2.3 V to 3.6 V. When $V_{CC} = 3.3$ V, the device can translate from a 5-V input to a 3.3-V output. In addition, when $V_{CC} = 3.3$ V the device can translate from 5-V or 3.3-V inputs to a 2.3-V output. The CB3T family can be used for voltage translation at moderately high frequencies. Figure 29 shows the simplified structure of the CB3T3306.
When the switch is on, the voltage at the gate of the NMOS pass transistor in the CB3T3306 is biased at $V_{CC} + V_T$, where $V_T$ is the threshold voltage of the NMOS. When input voltage starts to rise from low to high, the output follows the input voltage. As the input voltage reaches about one-half of $V_{CC}$, the control circuit senses this voltage and pulls the output voltage close to the $V_{CC}$ level and keeps the voltage constant as the input voltage increases. When the input reaches $V_{CC} + V_T$, the output voltage again increases to $V_{CC}$ and remains nearly flat, as the input voltage continues to rise. Input voltages at which these transitions occur depend on the output current, power supply, temperature, and transistor characteristics. The level of output high voltage ($V_{OH}$) also depends on the output current.

5.3.1 Characteristics of the CB3T Family

The following paragraphs discuss some of the critical performance characteristics of the CB3T3306. The measurements setup is given in Appendix A.

5.3.1.1 $V_O$ vs $V_I$

Figures 30 and 31 show the output voltage vs input voltage ($V_O$ vs $V_I$) characteristics of the CB3T3306 for different values of $V_{CC}$. The rapid increase in output voltage is due to the control circuit sensing the output voltage and pulling it high, close to the $V_{CC}$ level. The slope of this rapid rise in the curve depends on the output current being drawn from the switch.
Figure 31. $V_O$ vs $V_I$ in the CB3T3306 $I_O = -1 \mu A$ ($V_{CC} = 3.0$ V)

5.3.1.2 $r_{on}$ vs $V_I$

Figure 32 and Figure 33 shows the $r_{on}$ vs $V_I$ characteristics of the CB3T3306 at different $V_{CC}$ voltages. $r_{on}$ increases rapidly when the input voltage crosses approximately one-half of $V_{CC}$ and becomes flat above that voltage. The value of $r_{on}$ above that voltage depends greatly on the output current. As the output current increases, $r_{on}$ decreases.

Figure 32. $r_{on}$ vs $V_I$ for the CB3T3306 at $V_{CC} = 2.3$ V

Figure 33. $r_{on}$ vs $V_I$ for the CB3T3306 at $V_{CC} = 3.6$ V
5.3.1.3 Operation at High Frequency

CB3T devices can be used for voltage translation at moderately high frequencies. Figure 34 shows the operation of the CB3T3306 at 200 MHz. The load is 500 Ω and 3 pF to ground. Like the CB3Q family, the maximum I/O switching frequency depends on various factors, such as type of load, input signal magnitude, input signal edge rates, type of package, etc. With a larger package, the inductance and capacitance can form a resonant circuit that may cause phase and magnitude distortion. With a large capacitive load, the RC time constant becomes higher and limits the practical operating frequency.

![Input and Output Voltage Waveforms at 200 MHz (V_{CC} = 3.3 V)](image)

Figure 34. Input and Output Voltage Waveforms at 200 MHz (V_{CC} = 3.3 V)

5.3.2 Application of the CB3T Family

5.3.2.1 Voltage Translation for an External Monitor Terminal in a Notebook PC

Figure 35 shows a typical application for the level-translation feature of the CB3T3306. The CB3T3306 is used as a voltage translator between a monitor and a graphic controller. Data transfer between these two systems is bidirectional, while the clock signal transfer is unidirectional and flows only from graphic controller to monitor. Pullup resistors are used for translating from low to high.
Figure 35. Data and Clock-Signal Data Transfer Using the CB3T3306

6 Conclusion

TI’s CBT-C and CB3Q signal switches can be used for various types of high-speed applications, such as hot insertion for PCI interface, LAN signaling, \( \text{I}^2\text{C} \) bus expansion, video switching, etc. CB3T devices can be used for high-speed voltage translation in a mixed-voltage system. This application report has discussed some of the application performance characteristics of TI’s high-speed signal switches that are critical for the previously mentioned applications.

7 References

1. *Selecting the Right Texas Instruments Signal Switch*, John Perry and Chris Cockrill
2. *5-V to 3.3-V Translation With the SN74CBTD3384*, Nalin Yogasundram
Appendix A  Test Measurement Circuits

A.1  Measurement Setup for $r_{on}$

Figure A–1. $r_{on}$ Measurement Setup

A.2  Measurement Setup for $V_O$ vs $V_I$ Characteristics

Figure A–2. $V_O$ vs $V_I$ Measurement Setup
A.3 Voltage-Time Waveform Measurement (Switch On)

![Diagram](image1)

Figure A–3. Voltage-Time Waveform Measurement (Switch On)

A.4 Voltage-Time Waveform Measurement (Switch Off)

![Diagram](image2)

Figure A–4. Voltage-Time Waveform Measurement (Switch Off)
A.5 Output-Skew Measurement

![Diagram of Output-Skew Measurement Setup]

Figure A–5. Output-Skew Measurement Setup

A.6 Simulation Setup for Undershoot Measurement

![Diagram of SPICE Simulation Setup for Undershoot Measurement]

Figure A–6. SPICE Simulation Setup for Undershoot Measurement
A.7 Laboratory Setup for Attenuation Measurement

![Attenuation Measurement Setup Diagram]

Figure A–7. Attenuation Measurement Setup

A.8 Laboratory Setup for Off Isolation Measurement

![Off Isolation Measurement Setup Diagram]

Figure A–8. Off Isolation Measurement Setup
A.9 Laboratory Setup for Crosstalk Measurement

Figure A–9. Adjacent-Channel Crosstalk Measurement
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