



















THVD1505

JAJSHX3-SEPTEMBER 2019

THVD1505 IEC-ESD 保護機能およびバス極性訂正機能を備えた RS-485 トランシーバ

特長

- TIA/EIA-485A 規格、および SGCC (State Grid Corporation of China) Part 11 シリアル通信プロト コル RS-485 規格の要件を満たすか、それを上回 る性能
- 電源電圧:4.5V~5.5V
- 半二重 RS-422/RS-485
- 45ms 以内のバス極性訂正機能
- フェイルセーフ・バイアス抵抗あり/なしで動作
- データレート:最高 1Mbps
- バス I/O 保護
 - ±16kV HBM ESD
 - ±8kV IEC 61000-4-2 接触放電
 - ±8kV IEC 61000-4-2 エアギャップ放電
 - ±2kV IEC 61000-4-4 高速過渡バースト
- 開放、短絡、アイドル・バスのフェイルセーフ
- レシーバの大きなヒステリシスによるノイズ除 去:120mV
- 1 つのバスで最大 256 のノードに対応 (1/8 単位負
- 拡張周囲温度範囲:-40℃~125℃
- 低消費電力
 - スタンバイ時消費電流:1µA 未満
 - 動作時消費電流:1.1mA 未満
- グリッチなしの電源オン/オフによるホット・プラ グイン機能

2 アプリケーション

- 電気メータ
- HVAC システム
- インバータ
- ビデオ監視

3 概要

THVD1505 は、自動バス極性訂正機能と過渡保護機能 を備えた低消費電力の RS-485 トランシーバです。ホット プラグ時に、45ms 以内のバス・アイドル時間で、バス極性 の検出と訂正を行います。バスのピンは静電放電 (ESD) 事象に対する耐性を備えており、人体モデル (HBM)、 IEC 61000-4-2 接触放電およびエアギャップ放電の仕様 に関して高レベルの保護を実現しています。

差動ドライバと差動レシーバを組み合わせており、ともに 5Vの単一電源で動作します。ドライバの差動出力とレシー バの差動入力は内部的に接続され、半二重(2線式バス) 通信に適したバス・ポートを形成しています。 同相電圧範 囲が広いことから、このデバイスは長いケーブルを使用す るマルチポイント・アプリケーションに適しています。

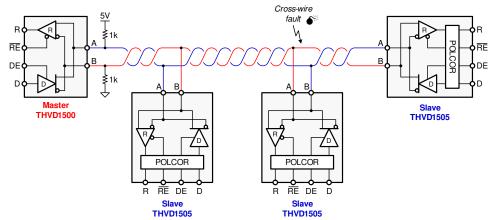
THVD1505 は SOIC-8 パッケージで供給され、-40℃~ 125℃の周囲温度範囲で仕様が規定されています。

製品情報(1)

型番	パッケージ	本体サイズ(公称)
THVD1505	SOIC (8)	4.90mm×3.91mm

(1) 利用可能なすべてのパッケージについては、このデータシートの末 尾にある注文情報を参照してください。

極性訂正機能(POLCOR)を備えた標準的なネットワーク・アプリケーション



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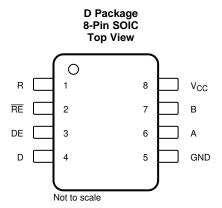
4 改訂履歴

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

日付	リビジョン	注	
2019 年 9 月	*	初版	



5 Pin Configuration and Functions



Pin Functions

PIN		I/O	DESCRIPTION		
NAME	NO.	1/0	DESCRIPTION		
А	6	Bus input/output	Driver output or receiver input (complementary to B)		
В	7	Bus input/output	Driver output or receiver input (complementary to A)		
D	4	Digital input	Driver data input (internal 5-MΩ pull-up)		
DE	3	Digital input	Driver enable, active high (internal 5-MΩ pull-down)		
GND	5	Ground	Device ground		
R	1	Digital output	Receive data output		
RE	2	Digital input	Receiver enable, active low (internal 5-M Ω pull-up)		
V _{cc}	8	Supply	4.5-V to 5.5-V supply		

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) (1)

		MIN	MAX	UNIT
V _{CC}	Supply voltage	-0.5	7	V
V_L	Input voltage at any logic pin (D, DE or RE)	-0.3	5.7	V
V _A , V _B	Voltage at A or B inputs, as differential or common-mode with respect to GND	-18	18	V
Io	Receiver output current	-24	24	mA
T_{J}	Junction temperature		170	°C
T _{STG}	Storage temperature	-65	150	°C

⁽¹⁾ Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditionsbeyond those indicated under Recommended Operating Conditions is not implied. Exposure to absolute-maximum-rated conditions forextended periods may affect device reliability.

6.2 ESD Ratings

				VALUE	UNIT
V _(ESD)		Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 (1)	Bus terminals and GND	±16,000	
		Human body model (HBM), per ANSI/ESDA/JEDEC 35-001	All other pins	±4,000	\ /
	Electrostatic discharge	Charged-device model (CDM), per JEDEC specification JESD22-0	C101 ⁽²⁾	±1,500	V
		Machine model (MM), per JEDEC JESD22-A115-A			

⁽¹⁾ JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

⁽²⁾ JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.



6.3 ESD Ratings [IEC]

			VALUE	UNIT
		IEC 61000-4-2 ESD contact discharge, bus terminals and GND	±8,000	
$V_{(ESD)}$	Electrostatic discharge	IEC 61000-4-2 ESD air-gap discharge, bus terminals and GND	±8,000	V
		IEC 61000-4-4 EFT fast transient, bus terminals and GND	±2,000	

6.4 Recommended Operating Conditions

			MIN	NOM	MAX	UNIT
V _{CC}	Supply voltage		4.5	5	5.5	V
V_{ID}	Differential input voltage		-12		12	V
VI	Input voltage at any bus termina	Input voltage at any bus terminal ⁽¹⁾			12	V
V _{IH}	High-level input voltage (driver, driver-enable, and receiver-enable inputs)		2		V _{CC}	V
V _{IL}	Low-level input voltage (driver, o	river-enable, and receiver-enable inputs)	0		0.8	V
	Output current	Driver	-60		60	mA
Io		Receiver	-8		8	
R_L	Differential load resistance		54	60		Ω
1/t _{UI}	Signaling rate	Signaling rate			1000	kbps
TJ	Junction temperature		-40		150	°C
T _A (2)	Operating ambient temperature	(see Thermal Information for additional information)	-40		125	°C

⁽¹⁾ The algebraic convention in which the least positive (most negative) limit is designated as minimum is used in this datasheet.

6.5 Thermal Information

		THVD1505	
	THERMAL METRIC ⁽¹⁾		UNIT
$R_{\theta JA}$	Junction-to-ambient thermal resistance	125.3	°C/W
R ₀ JC(top)	Junction-to-case (top) thermal resistance	67.6	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	68.6	°C/W
ΨЈТ	Junction-to-top characterization parameter	20.4	°C/W
ΨЈВ	Junction-to-board characterization parameter	67.8	°C/W

For more information about traditional and new thermalmetrics, see the Semiconductor and ICPackage Thermal Metrics application report.

⁽²⁾ Operation is specified for internal (junction) temperatures upto 150°C. Self-heating due to internal power dissipation should be considered for each application. Maximum junction temperature is internally limited by the thermal shutdown (TSD) circuit which disables the device when the junction temperature reaches 170°C.

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6.6 Electrical Characteristics

over operating free-air temperature range (unless otherwise noted)

	PARAMETER	TEST CONDITIO	ONS	MIN	TYP	MAX	UNIT
Driver							
		V _{test} from -7 to +12 V	See 🗵 7	1.5	2.5		
V _{OD}	Driver differential-output voltage magnitude	$R_L = 54 \Omega \text{ (RS-485)}, C_L = 50 \text{ pF}$	0 50	1.5	2.5		V
	magmitude	$R_L = 100 \Omega$ (RS-422), $C_L = 50 pF$	See 🗵 8	2	3		
Δ V _{OD}	Change in magnitude of driver differential-output voltage	$R_L = 54 \Omega, C_L = 50 pF$	See 🗵 8	-50		50	mV
V _{OC(SS)}	Steady-state common-mode output voltage			1	V _{CC} / 2	3	V
ΔV _{OC}	Change in differential driver common-mode output voltage	$R_L = 54 \Omega, C_L = 50 pF$	See 🗵 8	-50		50	mV
V _{OC(PP)}	Peak-to-peak driver common- mode output voltage				250		mV
I _{os}	Driver short-circuit output current	DE = V_{CC} , -7 V \leq [V_A or V_B] \leq 12 V, pin	or A pin shorted to B			150	mA
C _{OD}	Differential output capacitance				8		pF
Receiver							
I _I	Bus input current (driver disabled)	DE = 0 V, V _{CC} = 0 V or 5.5 V	V _I = 12 V		75	110	μA
I	Bus input current (univer disabled)	DE = 0 V, V _{CC} = 0 V 01 3.5 V	$V_1 = -7 V$	-90	-70		μА
R _A , R _B	Bus input impedance	$V_A = -7 \text{ V}, V_B = 12 \text{ V} \text{ and } V_A = 12 \text{ V}, V_B = -7 \text{ V}$	See 図 12	96			kΩ
V _{IT+}	Positive-going receiver differential-input voltage threshold				60	100	mV
V _{IT-}	Negative-going receiver differential-input voltage threshold			-100	-60		mV
V _{HYS} ⁽¹⁾	Receiver differential-input voltage threshold hysteresis $(V_{IT+} - V_{IT-})$			40	120		mV
V _{OH}	Receiver high-level output voltage	$I_{OH} = -8 \text{ mA}$		4	$V_{CC} - 0.3$		V
V _{OL}	Receiver low-level output voltage	I _{OL} = 8 mA			0.2	0.4	V
oz	Receiver high-impedance output current	$V_O = 0 \text{ V or } V_{CC}, \overline{RE} = V_{CC}$		-1		1	μΑ
OSR	Receiver output short-circuit current	$\overline{RE} = 0$, $DE = 0$	See 図 13			95	mA
Logic							
IN	Input current (D, DE, RE)			-2		2	μΑ
Supply							
		Driver and receiver enabled	$DE = V_{CC}, \overline{RE} = 0,$ no load		820	1100	
	Supply current (quiescent)	Driver enabled, receiver disabled	$ DE = V_{CC}, \overline{RE} = V_{CC}, \text{ no load} $		520	660	μA
lcc	Ouppry current (quiescent)	Driver disabled, receiver enabled	$DE = 0$, $\overline{RE} = 0$, no load		520	660	μА
		Driver and receiver disabled	$DE = 0$, $\overline{RE} = V_{CC}$, no load		0.03	1	

⁽¹⁾ Under any specific conditions, $V_{\text{IT+}}$ is specified to be at least V_{HYS} higher than $V_{\text{IT-}}$.



6.7 Power Dissipation Characteristics

PARAMETER		TEST CONDITIONS	VALUE	UNIT	
	Power dissipation, driver and		$R_L = 300 \Omega, C_L = 50 pF$	120	
	PD receiver enabled, $V_{CC} = 5.5 \text{ V}$, $T_A = 125^{\circ}\text{C}$, 50% duty cycle square-wave		$R_L = 100 \Omega, C_L = 50 pF$	160	mW
	signal at maximum signaling rate	RS-485 load	$R_L = 54 \Omega, C_L = 50 pF$	200	

6.8 Switching Characteristics

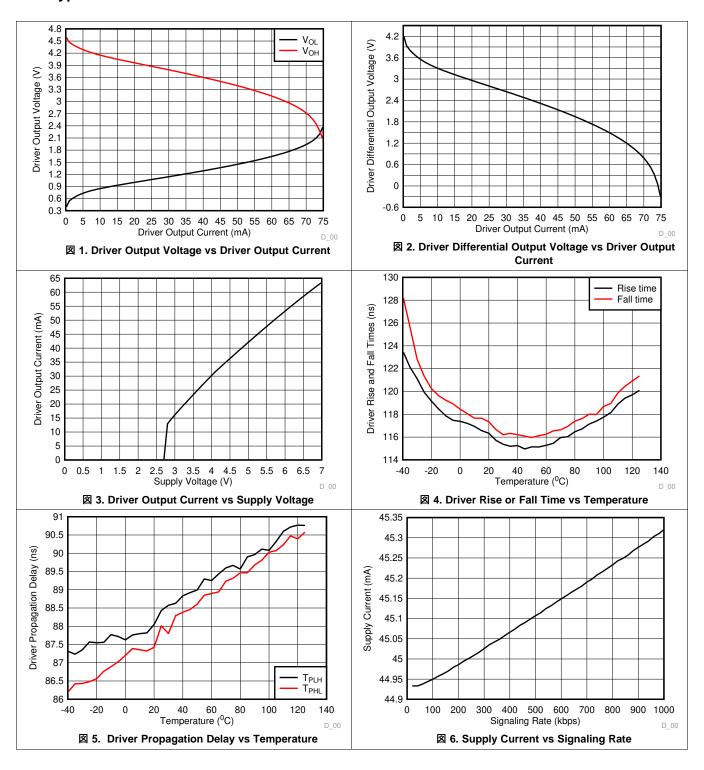
over operating free-air temperature range (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
Driver							
t _r , t _f	Driver differential output rise and fall times		See 🗵 9	100	115	300	ns
t _{PHL} , t _{PLH}	Driver propagation delay		See 🗵 9		90	350	ns
t _{SK(P)}	Driver pulse skew, t _{PHL} - t _{PLH}		See 🗵 9		25	40	ns
t _{PHZ} , t _{PLZ}	Driver disable time		See 図 10 and 図 11		70	160	ns
	Driver enable time	Receiver enabled	See 図 10 and 図 11		220	400	ns
t _{PHZ} , t _{PLZ}		Receiver disabled	See 図 10 and 図 11		1.5	3	μs
Receiver						"	
t _r , t _f	Receiver output rise and fall times		See 🗵 14		6	30	ns
t _{PHL} , t _{PLH}	Receiver propagation delay time		See 🗵 14		80	120	ns
t _{SK(P)}	Receiver pulse skew, t _{PHL} - t _{PLH}		See 🗵 14		2	7	ns
t _{PHZ} , t _{PLZ}	Receiver disable time		See 図 15		15	30	ns
t _{PZL(1)} ,		Driver enabled	See 🗵 15		180	370	ns
$t_{PZH(1)}$ $t_{PZL(2)}$, $t_{PZH(2)}$	Receiver enable time	Driver disabled	See 図 16		1	5	μs
t _{FS}	Bus fail-safe time	Driver disabled	See 🗵 17	25	35	45	ms



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6.9 Typical Characteristics



7 Parameter Measurement Information

7.1 Driver

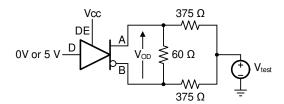
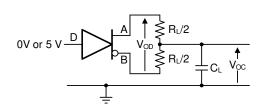


図 7. Measurement of Driver Differential-Output Voltage With Common-Mode Load



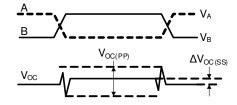
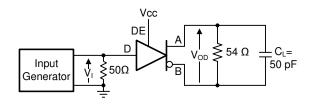


図 8. Measurement of Driver Differential and Common-Mode Output With RS-485 Load



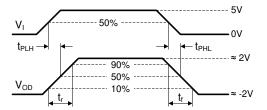
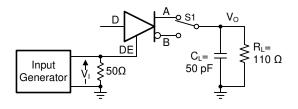


図 9. Measurement of Driver Differential-Output Rise and Fall Times and Propagation Delays



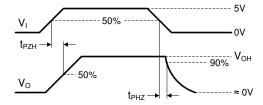
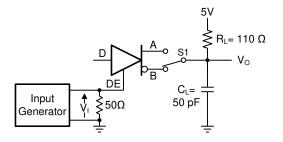


図 10. Measurement of Driver Enable and Disable Times With Active-High Output and Pull-Down Load



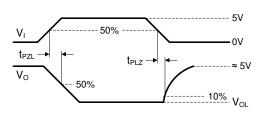


図 11. Measurement of Driver Enable and Disable Times With Active-Low Output and Pull-up Load

7.2 Receiver

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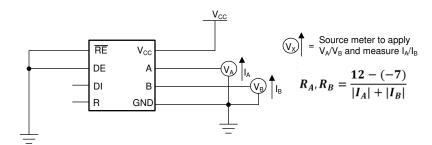


図 12. Measurement of Bus Impedance

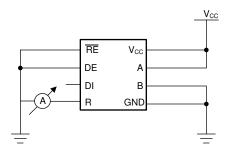


図 13. Measurement of Receiver Output Short Circuit Current

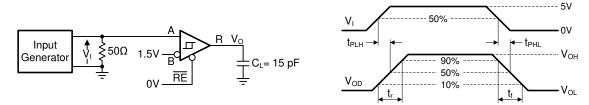


図 14. Measurement of Receiver Output Rise and Fall Times and Propagation Delays

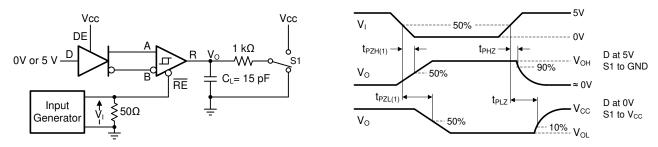


図 15. Measurement of Receiver Enable and Disable Times With Driver Enabled

Receiver (continued)

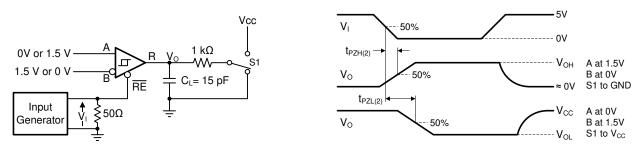


図 16. Measurement of Receiver Enable Times With Driver Disabled

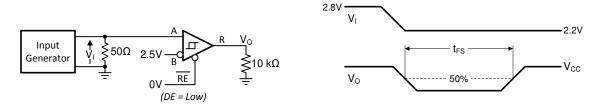


図 17. Measurement of Receiver Polarity-Correction Time With Driver Disabled

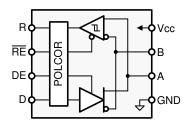
8 Detailed Description

8.1 Overview

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The THVD1505 device is a half-duplex RS-485 transceiver suitable for data transmission at rates up to 1 Mbps over controlled-impedance transmission media (such as twisted-pair cabling). The device features a high level of internal transient protection, making it able to withstand ESD strikes up to ±8 kV (per IEC 61000-4-2) and EFT transients up to ±2 kV (per IEC 61000-4-4) without incurring damage. Up to 256 units of THVD1500 and/or THVD1505 may share a common RS-485 bus due to the devices' low bus input currents. THVD1505 features automatic polarity correction, which detects bus mis-wiring and swaps A and B.

8.2 Functional Block Diagram



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8.3 Feature Description

8.3.1 Bus Polarity Correction

THVD1505 automatically corrects a wrong bus-signal polarity caused by a mis-wire fault. In order to detect the bus polarity, the following conditions must be met.

- A slave node must enable the receiver (RE = low). Driver can be in either enabled or disabled state
- A and B signals should be static for longer than fail-safe time (t_{ES})
- The absolute value of the differential voltage at the receiver input should be greater than the receiver thresholds (|V_{IT+}| or |V_{IT-}|)

The receiver input voltage can be defined either by using passive fail-safe resistors or by the master node actively driving the bus.

8.3.1.1 Passive Polarity Definition Using Fail-Safe Biasing Network

🗵 18 shows a simple point-to-point data link between a master node and a slave node with mis-wire fault.

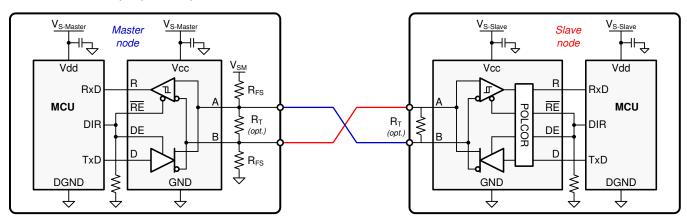


図 18. Passive Polarity Definition

Feature Description (continued)

During passive polarity definition, an external fail-safe resistor network (R_{FS}) must be used to ensure fail-safe operation during an idle bus state. When the bus is not actively driven, the differential receiver inputs could float allowing the receiver output to assume a random output. A proper fail-safe network forces the receiver inputs to exceed the V_{IT} threshold, thus forcing the THVD1505 receiver output into the high state.

2 19 shows the timing diagram for passive polarity definition.

Prior to initiating data transmission the master transceiver must idle for a time span that exceeds the maximum fail-safe time, t_{FS} , of a slave transceiver. This idle time is accomplished by driving the direction control line (the output of the MCU in \boxtimes 19 that is driving DE and \overline{RE} pins), DIR, low. After a time, $t > t_{FS}$, the master begins transmitting data.

Because of the indicated mis-wire fault between master and slave, the slave node receives bus signals with reversed polarity. Assuming the slave node has just been connected to the bus, the direction-control pin is pulled-down during power-up and then is actively driven low by the slave MCU. The polarity correction begins as soon as the slave supply is established and ends after t_{FS}.

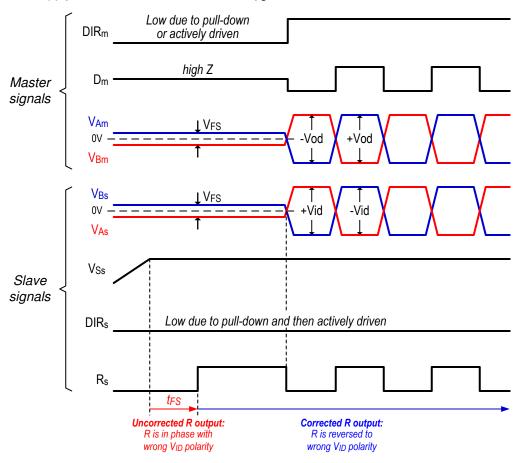


図 19. Polarity Correction Timing With Passive Polarity Definition

Initially, the slave receiver assumes that the correct bus polarity is applied to the inputs and performs no polarity reversal. Because of the reversed polarity of the bus-failsafe voltage, the output of the slave receiver, R_S , turns low. After t_{FS} has passed and the receiver has detected the wrong bus polarity, the internal POLCOR logic reverses the input signal and R_S turns high.

At this point, all incoming bus data with reversed polarity are polarity corrected within the transceiver. Because polarity correction is also applied to the transmit path, the data sent by the slave MCU are reversed by the POLCOR logic and then fed into the driver.



Feature Description (continued)

The reversed data from the slave MCU are reversed again by the mis-wire fault in the bus, and the correct bus polarity is reestablished at the master end.

THVD1505 retains the state of the polarity logic as long as V_{CC} is present to the device. However, the device POLCOR logic powers up in the default no polarity reversal mode at each device power up. POLCOR logic remains active as long as V_{CC} is applied to the device.

注

Data string durations of consecutive 0s or 1s exceeding the minimum t_{FS} can accidently trigger a wrong polarity correction and must be avoided.

8.3.1.2 Active Polarity Definition by the Master Node

THVD1505 polarity correction can also work without a fail-safe resistor network. See 22.

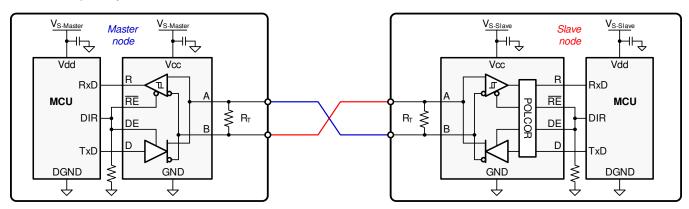


図 20. Active Polarity Definition

In this scenario, the master node drives the bus for longer than t_{FS} . After a time, $t > t_{FS}$, the master begins transmitting data. 21 shows the timing diagram for active polarity definition. DIR pin refers to the output of the MCU that is driving DE and \overline{RE} pins in 21.

Feature Description (continued)

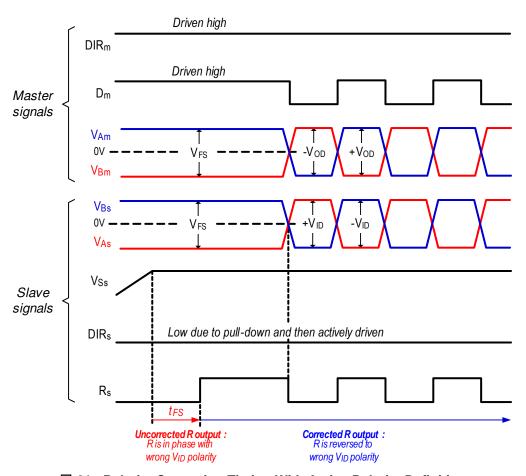


図 21. Polarity Correction Timing With Active Polarity Definition

POLCOR logic behavior with active polarity definition is identical to the POLCOR logic behavior with passive polarity definition.



8.4 Device Functional Modes

表 1. Driver Pin Functions

INPUT	ENABLE	OUTPUTS		DESCRIPTION			
D	DE	Α	В	DESCRIPTION			
NORMAL MO	DDE						
Н	Н	Н	L	Actively drives bus high			
L	Н	L	Н	Actively drives bus low			
Х	L	Z	Z	Driver disabled			
Х	OPEN	Z	Z	Driver disabled by default			
OPEN	Н	Н	L	Actively drives bus high			
POLARITY-C	ORRECTING MOD	E					
Н	Н	L	Н	Actively drives bus low			
L	Н	Н	L	Actively drives bus high			
Х	L	Z	Z	Driver disabled			
Х	OPEN	Z Z		Driver disabled by default			
OPEN	Н	L	Н	Actively drives bus low			

表 2. Receiver Pin Functions

DIFFERENTIAL INPUT	EN	ABLE	ОИТРИТ	DESCRIPTION				
$V_{ID} = V_A - V_B$	RE DE		R					
$V_{\text{ID}} > V_{\text{IT+}}$	L X		Н	Receive valid bus high				
$V_{IT-} > V_{ID}$	L X		L during t _{FS} H after t _{FS}	Receive valid bus low if lasting for less than $t_{\text{FS}},$ polarity correcting if lasting for more than t_{FS}				
X	н х		Z	Receiver disabled				
X	OPEN	Х	Z	Receiver disabled				
Open, short or V _{IT+} > V _{ID} > V _{IT-}	L X		H after t _{FS}	Receiver fail-safe high				

9 Application and Implementation

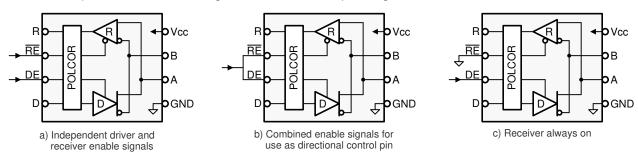
注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

9.1 Application Information

9.1.1 Device Configuration

The THVD1505 is a half-duplex RS-485 transceiver operating from a single 5-V ±10% supply. The driver and receiver enable pins allow for the configuration of different operating modes.



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図 22. Transceiver Configurations

Using independent enable lines provides the most flexible control as the lines allow for the driver and the receiver to be turned on and turned off individually. While this configuration requires two control lines, it allows for selective listening to the bus traffic, whether the driver is transmitting data or not. Only this configuration allows the THVD1505 to enter low-power standby mode because it allows both the driver and receiver to be disabled simultaneously.

Combining the enable signals simplifies the interface to the controller by forming a single direction-control signal. Thus, when the direction-control line is high, the transceiver is configured as a driver, while for a low the device operates as a receiver.

Tying the receiver enable to ground and controlling only the driver-enable input also uses only one control line. In this configuration, a node not only receives the data on the bus sent by other nodes but also receives the data sent on the bus, enabling the node to verify the correct data has been transmitted.

9.1.2 Bus Design

An RS-485 bus consists of multiple transceivers connected in parallel to a bus cable. To eliminate line reflections, each cable end is terminated with a termination resistor, R_T , whose value matches the characteristic impedance, Z_0 , of the cable. This method, known as parallel termination, allows for relatively high data rates over long cable length.

Common cables used are unshielded twisted pair (UTP), such as low-cost CAT-5 cable with Z_0 = 100 Ω , and RS-485 cable with Z_0 = 120 Ω . Typical cable sizes are AWG 22 and AWG 24.

The maximum bus length is typically given as 4000 ft or 1200 m, and represents the length of an AWG 24 cable whose cable resistance approaches the value of the termination resistance, thus reducing the bus signal by half or 6 dB. Actual maximum usable cable length depends on the signaling rate, cable characteristics, and environmental conditions.

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Application Information (continued)

9.1.3 Fail-Safe Biasing for Passive Polarity Definition

External biasing resistor network of R_{FS} along with R_T define the V_{FS} during the polarity correction time, t_{FS}. See Passive Polarity Definition Using Fail-Safe Biasing Network for more details.

 R_{FS} resistors should be selected such that $V_{FS} > |V_{IT}| = 100$ mV. The equation below can be used to calculate R_{FS}. Note that too low of a R_{FS} value increases the bus loading that reduces the number of nodes on the RS-485 bus.

$$R_{FS} < 0.5 \times [(R_T \times V_{CC-min}) / 0.1 - R_T]$$
 (1)

9.1.4 Cable Length Versus Data Rate

There is an inverse relationship between data rate and cable length, which means the higher the data rate, the shorter the cable length; and conversely, the lower the data rate the longer the cable length. While most RS-485 systems use data rates between 10 kbps and 100 kbps, applications such as e-metering often operate at rates of up to 250 kbps even at distances of 4000 ft and longer. Longer distances are possible by allowing for small signal jitter of up to 5 or 10%.

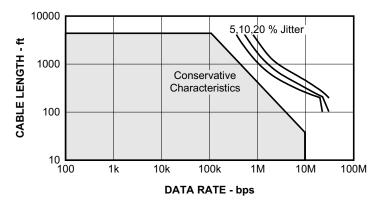


図 23. Cable Length vs Data Rate Characteristic

9.1.5 Stub Length

When connecting a node to the bus, the distance between the transceiver inputs and the cable trunk, known as the stub, should be as short as possible. The reason for the short distance is because a stub presents a nonterminated piece of bus line which can introduce reflections if the distance is too long. As a general guideline, the electrical length or round-trip delay of a stub should be less than one-tenth of the rise time of the driver, thus leading to a maximum physical stub length of as shown in 式 2.

$$L_S \le 0.1 \times t_r \times v \times c$$

where

- t_r is the 10/90 rise time of the driver
- c is the speed of light (3 \times 10⁸ m/s or 9.8 \times 10⁸ ft/s)
- v is the signal velocity of the cable (v = 78%) or trace (v = 45%) as a factor of c (2)

Based on 式 2, with a minimum rise time of 400 ns, 式 3 shows the maximum cable-stub length of the THVD1505.

$$L_S \le 0.1 \times 400 \times 10^{-9} \times 3 \cdot 10^8 \times 0.78 = 9.4 \text{ m (or } 30.6 \text{ ft)}$$
 (3)

Application Information (continued)

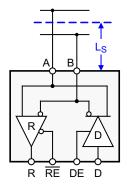


図 24. Stub Length

9.1.6 Transient Protection

The bus terminals of the THVD1505 transceiver family possess on-chip ESD protection against ± 16 kV HBM, ± 8 kV IEC 61000-4-2 contact discharge and ± 2 kV IEC 61000-4-4 EFT. The International Electrotechnical Commission (IEC) ESD test is far more severe than the HBM ESD test. The 50% higher charge capacitance, C_S, and 78% lower discharge resistance, R_D of the IEC model produce significantly higher discharge currents than the HBM model.

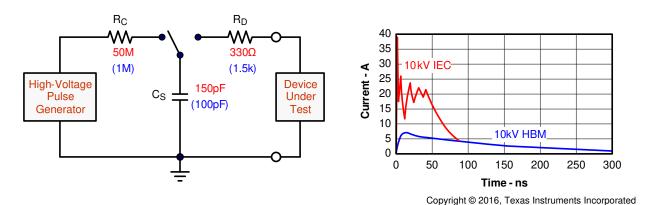


図 25. HBM and IEC ESD Models and Currents in Comparison (HBM Values in Parenthesis)

The on-chip implementation of IEC ESD and EFT protection significantly increases the robustness of equipment. Common discharge events occur because of human contact with connectors and cables. EFTs are generally caused by relay-contact bounce or the interruption of inductive loads.

Surge transients often result from lightning strikes (direct strike or an indirect strike which induce voltages and currents), or the switching of power systems, including load changes and short circuit switching. These transients are often encountered in industrial environments, such as factory automation and power-grid systems.

№ 26 compares the pulse-power of the EFT and surge transients with the power caused by an IEC ESD transient. The left hand diagram shows the relative pulse-power for a 0.5-kV surge transient and 4-kV EFT transient, both of which dwarf the 10-kV ESD transient visible in the lower-left corner. 500-V surge transients are representative of events that may occur in factory environments in industrial and process automation. The right hand diagram shows the pulse-power of a 6-kV surge transient, relative to the same 0.5-kV surge transient. 6-kV surge transients are most likely to occur in power generation and power-grid systems.

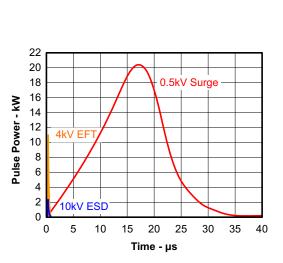
Designers may choose to implement protection against longer duration surge transients. 図 28 suggests two circuit designs providing protection against short and long duration surge transients. 表 3 lists the bill of materials for the external protection devices.



Application Information (continued)

注

The unit of the pulse-power changes from kW to MW, thus making the power of the 500-V surge transient almost dropping off the scale.



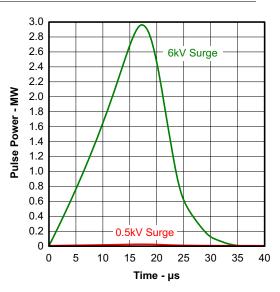


図 26. Power Comparison of ESD, EFT, and Surge Transients

In the case of surge transients, high-energy content is signified by long pulse duration and slow decaying pulse power.

The electrical energy of a transient that is dumped into the internal protection cells of the transceiver is converted into thermal energy. This thermal energy heats the protection cells and literally destroys them, thus destroying the transceiver.

27 shows the large differences in transient energies for single ESD, EFT, and surge transients as well as for an EFT pulse train, commonly applied during compliance testing.

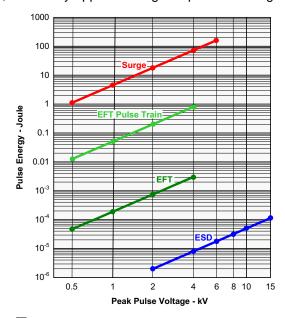


図 27. Comparison of Transient Energies

TEXAS INSTRUMENTS

Application Information (continued)

表 3. List of Components

DEVICE	FUNCTION	ORDER NUMBER (1)	MANUFACTURER
XCVR	5-V, 1-Mbps RS-485 Transceiver	THVD1505DR	TI
R1, R2	10-Ω, Pulse-Proof Thick-Film Resistor	CRCW0603010RJNEAHP	Vishay
TVS	Bidirectional 400-W Transient Voltage Suppressor	CDSOT23-SM712	Bourns
TBU1, TBU2	Bidirectional 200mA Transient Blocking Unit	TBU-CA-065-200-WH	Bourns
MOV1, MOV2	200-mA Transient Blocking Unit 200-V, Metal-Oxide Varistor	MOV-10D201K	Bourns

(1) See Third Party Disclaimer

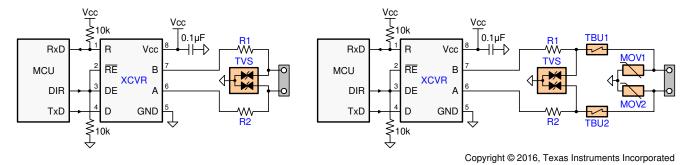


図 28. Transient Protections Against Surge Transients

The left circuit shown in \boxtimes 28 provides surge protection of 1-kV transients, while the right protection circuits can withstand surge transients of 5 kV.



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9.2 Typical Application

Many RS-485 networks use isolated bus nodes to prevent the creation of unintended ground loops and their disruptive impact on signal integrity. An isolated bus node typically includes a micro controller that connects to the bus transceiver through a multi-channel, digital isolator (2).

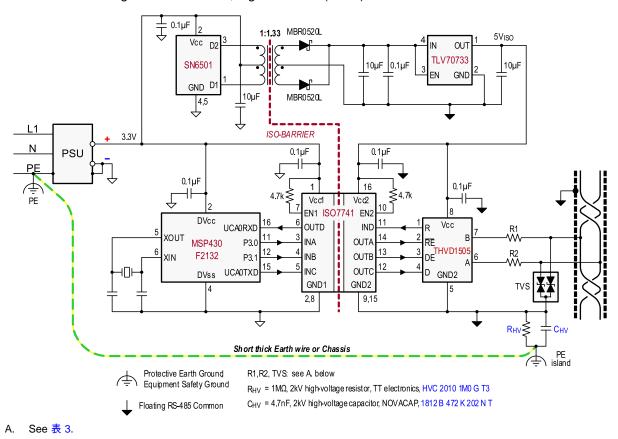


図 29. Isolated Bus Node With Transient Protection

9.2.1 Design Requirements

Example Application: Isolated Bus Node with Transient Protection

- RS-485-compliant bus interface.
- Galvanic isolation of both signal and power supply lines.
- Able to withstand surge transients up to 1 kV (per IEC 61000-4-5).
- Full control of data flow on bus in order to prevent contention (for half-duplex communication).

9.2.2 Detailed Design Procedure

Power isolation is accomplished using the push-pull transformer driver SN6501, a low-cost LDO and TLV70733.

Signal isolation uses the quadruple digital isolator ISO7741. Notice that both enable inputs, EN1 and EN2, are pulled-up via 4.7-k Ω resistors to limit input currents during transient events.

While the transient protection is similar to the one in **2** 28 (left circuit), an additional high-voltage capacitor diverts transient energy from the floating RS-485 common further towards protective earth (PE) ground. This diversion is necessary as noise transients on the bus are usually referred to Earth potential.

R_{VH} refers to a high-voltage resistor, and in some applications even a varistor. This resistance is applied to prevent charging of the floating ground to dangerous potentials during normal operation.

Occasionally varistors are used instead of resistors in order to rapidly discharge C_{HV} , if expected that fast transients might charge C_{HV} to high-potentials.

TEXAS INSTRUMENTS

Typical Application (continued)

Note that the PE island represents a copper island on the PCB for the provision of a short, thick Earth wire connecting this island to PE ground at the entrance of the power supply unit (PSU).

In equipment designs using a chassis, the PE connection is usually provided through the chassis itself. Typically the PE conductor is tied to the chassis at one end while the high-voltage components, C_{HV} and R_{HV} , are connecting to the chassis at the other end.

9.2.3 Application Curve

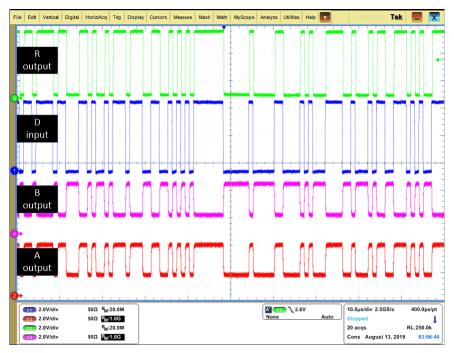


図 30. Waveforms at 1 Mbps Operation, PRBS7 Data Pattern

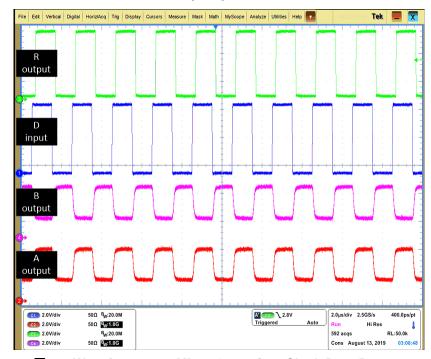


図 31. Waveforms at 1 Mbps Operation, Clock Data Pattern



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10 Power Supply Recommendations

To ensure reliable operation at all data rates and supply voltages, each supply should be decoupled with a 100-nF ceramic capacitor located as close to the supply pins as possible. This helps to reduce supply voltage ripple present on the outputs of switched-mode power supplies and also helps to compensate for the resistance and inductance of the PCB power planes.

11 Layout

11.1 Layout Guidelines

11.1.1 Design and Layout Considerations For Transient Protection

Robust and reliable bus node design often requires the use of external transient protection devices in order to protect against surge transients that may occur in industrial environments. Since these transients have a wide frequency bandwidth (from approximately 3 MHz to 300 MHz), high-frequency layout techniques should be applied during PCB design.

- 1. Place the protection circuitry close to the bus connector to prevent noise transients from propagating across the board.
- 2. Use Vcc and ground planes to provide low inductance. Note that high frequency currents follow the path of least impedance and not the path of least resistance.
- 3. Design the protection components into the direction of the signal path. Do not force the transients currents to divert from the signal path to reach the protection device.
- Apply 100 to 220-nF decoupling capacitors as close as possible to the V_{CC} pins of transceiver and UART or controller ICs on the board.
- 5. Use at least two vias for V_{CC} and ground connections of decoupling capacitors and protection devices to minimize effective via inductance.
- 6. Use 1 to 10-k pull-up or pull-down resistors for enable lines to limit noise currents in theses lines during transient events.
- 7. Insert pulse-proof resistors into the A and B bus lines if the TVS clamping voltage is higher than the specified maximum voltage of the transceiver bus terminals. These resistors limit the residual clamping current into the transceiver and prevent it from latching up.
 - While pure TVS protection is sufficient for surge transients up to 1 kV, higher transients require metaloxide varistors (MOVs) which reduce the transients to a few-hundred volts of clamping voltage, and transient blocking units (TBUs) that limit transient current to about 200 mA.

11.2 Layout Example

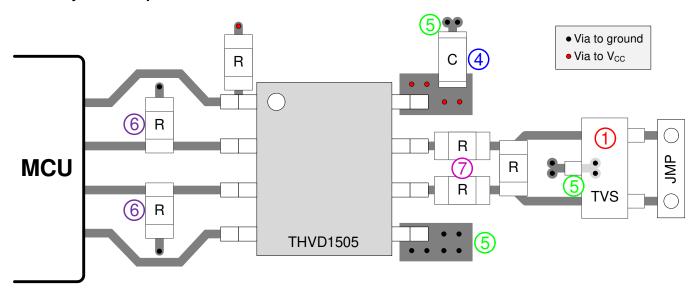


図 32. THVD1505 Layout Example



12 デバイスおよびドキュメントのサポート

12.1 デバイス・サポート

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12.6 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

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PACKAGE OPTION ADDENDUM

10-Dec-2020

PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead finish/ Ball material	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
							(6)				
THVD1505DR	ACTIVE	SOIC	D	8	2500	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	1505	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

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- (3) MSL, Peak Temp. The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- (5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- (6) Lead finish/Ball material Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	_	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
THVD1505DR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1

PACKAGE MATERIALS INFORMATION

www.ti.com 3-Jun-2022



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
THVD1505DR	SOIC	D	8	2500	356.0	356.0	35.0



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES:

- 1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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